

The first part of this problem is identical to HW Problem (Jackson 7.2)

Let \vec{E}_0 be along x-axis, incident wave vector \vec{k}_1 along z-axis. $E_z = E_0$

Electric field is given by (leaving out common $e^{-i\omega t}$ factor).

Region (1) $(E_0 e^{ik_1 z} + E_r e^{-ik_1 z}) \vec{e}_0$

Region (2) $(E_i(2) e^{ik_2 z} + E_r(2) e^{-ik_2 z}) \vec{e}_0$

Region (3) $E_t(3) e^{ik_1 z} \vec{e}_0$

(because $k = n \frac{\omega}{c}$, wave vector in region (3) = wave vector in region (1))

Assume all μ 's are $\approx \mu_0$ $n_2 = \sqrt{\frac{\epsilon(\omega)}{\epsilon_0}}$ $k_2 = n_2 k_1$ $k_1 = \frac{\omega}{c}$

Boundary conditions at $z=0$

$E_0 + E_r = E_i(2) + E_r(2)$ (from tangential \vec{E} field)

$E_0 - E_r = n_2 (E_i(2) - E_r(2))$ (from tangential \vec{H} field)

so $\begin{pmatrix} E_i(2) \\ E_r(2) \end{pmatrix} = \underline{t}_1 \begin{pmatrix} E_0 \\ E_r \end{pmatrix}$; $\underline{t}_1 = \begin{pmatrix} \frac{(1+n_2)}{2n_2} & \frac{(n_2-1)}{2n_2} \\ \frac{(n_2-1)}{2n_2} & \frac{1+n_2}{2n_2} \end{pmatrix}$

Boundary conditions at $z=d$

$E_i(2) e^{ik_2 d} + E_r(2) e^{-ik_2 d} = E_t(3) e^{ik_1 d}$

$n_2 (E_i(2) e^{ik_2 d} - E_r(2) e^{-ik_2 d}) = E_t(3) e^{ik_1 d}$

or $\begin{pmatrix} E_t(3) \\ 0 \end{pmatrix} = \underline{t}_2 \begin{pmatrix} E_i(2) \\ E_r(2) \end{pmatrix}$ $\underline{t}_2 = \begin{pmatrix} \frac{n_2+1}{2} e^{i(k_2-k_1)d} & \frac{1-n_2}{2} e^{i(k_2+k_1)d} \\ \frac{1-n_2}{2} e^{i(k_2-k_1)d} & \frac{1+n_2}{2} e^{-i(k_2+k_1)d} \end{pmatrix}$

$$\Rightarrow \begin{pmatrix} E_r(z) \\ 0 \end{pmatrix} = T \begin{pmatrix} E_0 \\ E_r \end{pmatrix} = \begin{pmatrix} T_{11} & T_{12} \\ T_{21} & T_{22} \end{pmatrix} \begin{pmatrix} E_0 \\ E_r \end{pmatrix} \quad (1)$$

$$T = \begin{matrix} t_2 & t_1 \\ s & s \end{matrix}, \quad \text{with } k_2 = n_2 k_1$$

$$\left. \begin{aligned} T_{11} &= \frac{(n_2+1)(1+n_2)}{2} \frac{e^{i(n_2-1)k_1 d}}{2n_2} + \frac{(1-n_2)(n_2-1)}{2} \frac{e^{-i(n_2+1)k_1 d}}{2n_2} \\ T_{12} &= \frac{(n_2+1)(n_2-1)}{2} \frac{e^{i(n_2-1)k_1 d}}{2n_2} + \frac{(1-n_2)(1+n_2)}{2} \frac{e^{-i(n_2+1)k_1 d}}{2n_2} \\ T_{21} &= \frac{(1-n_2)(1+n_2)}{2} \frac{e^{i(n_2-1)k_1 d}}{2n_2} + \frac{(n_2+1)(n_2-1)}{2} \frac{e^{i(n_2+1)k_1 d}}{2n_2} \\ T_{22} &= \frac{(1-n_2)(n_2-1)}{2} \frac{e^{i(n_2-1)k_1 d}}{2n_2} + \frac{(n_2+1)(n_2+1)}{2} \frac{e^{-i(n_2+1)k_1 d}}{2n_2} \end{aligned} \right\} (2)$$

From Eqs (1)

$$E_r = - \frac{T_{21}}{T_{22}} E_0 = r E_0$$

$$E_t(z) = \left[T_{11} - \frac{T_{12} T_{21}}{T_{22}} \right] E_0 = t E_0$$

$$\text{so transmitted wave} = \vec{e}_0 E_0 e^{i k_1 z} \left[T_{11} - \frac{T_{12} T_{21}}{T_{22}} \right]$$

$$\text{Now by Eqs (2), } T_{11} = \frac{(1+n_2)^2}{4n_2} e^{i(n_2-1)k_1 d} - \frac{(1-n_2)^2}{4n_2} e^{-i(n_2+1)k_1 d}$$

$$\left(\text{Expanding exponentials to 1st order in } d \right) = \frac{(1+n_2)^2}{4n_2} [1 + i(n_2-1)k_1 d] - \frac{(1-n_2)^2}{4n_2} [1 - i(n_2+1)k_1 d]$$

$$\text{after some algebra} = 1 + i(n_2^2 - 1) \frac{k_1 d}{2}$$

$$\begin{aligned} T_{12} &= \frac{(n_2^2-1)}{4n_2} e^{i(n_2-1)k_1 d} - \frac{(n_2^2-1)}{4n_2} e^{-i(n_2+1)k_1 d} \\ &\approx \frac{(n_2^2-1)}{4n_2} [1 + i(n_2-1)k_1 d - 1 + i(n_2+1)k_1 d] \\ &= \frac{(n_2^2-1)}{4n_2} 2i n_2 k_1 d = i \frac{(n_2^2-1)}{2} k_1 d \end{aligned}$$

$$T_{21} = \frac{(1-n_2^2)}{4n_2} e^{i(n_2-1)k_1 d} + \frac{(n_2^2-1)}{4n_2} e^{i(n_2+1)k_1 d}$$

$$= -T_{12} \approx -i \frac{(n_2^2-1)k_1 d}{2}$$

$$T_{33} = -\frac{(n_2-1)^2}{4n_2} e^{i(n_2-1)k_1 d} + \frac{(n_2+1)^2}{4n_2} e^{-i(n_2+1)k_1 d}$$

$$\approx -\frac{(n_2-1)^2}{4n_2} [1 + i(n_2-1)k_1 d] + \frac{(n_2+1)^2}{4n_2} [1 - i(n_2+1)k_1 d]$$

$$= 1 - i k d \frac{(n_2^2+3)}{2}$$

so $\frac{T_{12} T_{21}}{T_{22}} \sim O(d^2)$

to order d ,

$$\vec{E}_t = \vec{e}_0 E_0 e^{i k_1 z} \left[1 + i \frac{(n_2^2-1) k d}{2} \right]$$

$$= \vec{e}_0 E_0 e^{i k_1 z} \left[1 + i \left(\frac{\epsilon(\omega)}{\epsilon_0} - 1 \right) \frac{k d}{2} \right] \quad (3a)$$

$$\vec{E}_r = \vec{e}_0 E_0 e^{-i k_1 z} \left(\frac{T_{21}}{T_{22}} \right) = \vec{e}_0 E_0 e^{-i k_1 z} \left[i \frac{(n_2^2-1) k d}{2} \right] = \vec{e}_0 E_0 e^{-i k_1 z} \left[i \left(\frac{\epsilon(\omega)}{\epsilon_0} - 1 \right) \frac{k d}{2} \right]$$

(b) If we define the magnitudes of the Poynting vectors of the incident, reflected + transmitted waves as

$$I_1 = \frac{1}{2Z_0} |\vec{E}_i|^2 ; I_2 = \frac{1}{2Z_0} |\vec{E}_r|^2 ; I_3 = \frac{1}{2Z_0} |\vec{E}_t|^2$$

($Z_0 =$ Impedance of free space)

then the rate of power dissipation per unit area in the slab

$$P_{abs} = I_1 - I_2 - I_3 = \frac{1}{2Z_0} \left[E_0^2 - |\vec{E}_t|^2 - |\vec{E}_r|^2 \right] \quad (4)$$

Because of the conductivity $\frac{\epsilon(\omega)}{\epsilon_0}$ has an imaginary part:

$$\frac{\epsilon(\omega)}{\epsilon_0} = \epsilon_f(\omega) + i \frac{\sigma(\omega)}{\omega} \quad (\text{Jackson Eq (7.56)}) \quad (5)$$

where $\epsilon_f(\omega)$ can be considered as real + the bound part + $\sigma(\omega)$ is the conductivity. Because of the form of Eq. (2) we must consider possible terms of $O(d^2)$ in E_t and E_r .

Thus we write

$$\vec{E}_t = \vec{e}_0 E_0 e^{i k_1 z} \left[1 + i \left(\frac{\epsilon_f}{\epsilon_0} - 1 \right) \frac{k d}{2} - \frac{\sigma}{\epsilon_0 \omega} \frac{k d}{2} + O(d^2) \right]$$

$$|\vec{E}_t|^2 = |E_0|^2 \left[1 - \frac{\sigma}{\epsilon_0 \omega} k d \right] \text{ to leading order in } d.$$

From Eq. (3B), $|E_r|^2 \sim O(d^2)$ so we can neglect it to leading order in d ,

$$P_{\text{abs}} = \frac{|E_0|^2 \sigma}{2Z_0 \epsilon_0 \omega} k d = \frac{1}{2Z_0 \epsilon_0} \sigma d \quad (\omega/k = c)$$

$$= \frac{1}{2} \sqrt{\frac{\epsilon_0}{\mu_0}} \frac{\sigma}{\epsilon_0} \sqrt{\mu_0 \epsilon_0} d |E_0|^2 = \boxed{\frac{1}{2} |E_0|^2 \sigma d}$$

NVE: We could also have got this result by recognizing that ^{time-averaged} power dissipated per unit volume in conductor $= \frac{1}{2} \mathbf{J} \cdot \mathbf{E} = \frac{1}{2} \sigma |\mathbf{E}|^2$ (only true to lowest order since it assumes field in conductor is incident field)

2.

(a) Eqns of motion for electron is

$$m \left[\ddot{\vec{x}} + \gamma \dot{\vec{x}} + \omega_0^2 \vec{x} \right] - e \vec{B}_0 \times \dot{\vec{x}} = -e \vec{E} e^{-i\omega t} \quad (\vec{B}_0 \text{ along } z)$$

Write electric field \vec{E} as a circularly polarized (+) wave

$$\vec{E} = E_0 (\vec{e}_1 + i\vec{e}_2)$$

Choose solutions of form $\vec{x} = \vec{x}_0 (\vec{e}_1 + i\vec{e}_2) e^{-i\omega t}$ (\vec{e}_1, \vec{e}_2 along x, y)

so we get $[m\omega^2 - i\gamma m\omega + m\omega_0^2] \vec{x}_0 (\vec{e}_1 + i\vec{e}_2)$

$$+ i\omega e B_0 \times \vec{x}_0 (\vec{e}_1 + i\vec{e}_2) = -e E_0 (\vec{e}_1 + i\vec{e}_2)$$

Equating coeff. of \vec{e}_1 ,

$$m(\omega_0^2 - \omega^2 - i\gamma\omega) x_0 \pm e B_0 \omega x_0 = -e E_0$$

or $x_0 = -\frac{e}{m} \frac{E_0}{\omega_0^2 - \omega^2 - i\gamma\omega \pm e B_0 \omega / m}$

of \vec{e}_2 gives same solution

$$\Rightarrow \vec{P}_{\pm} = -e \vec{X}_{\pm} = \frac{e^2}{m} \frac{1}{\omega_0^2 - \omega^2 - i\gamma\omega \pm e B_0 \omega / m}$$

$$\Rightarrow \left[\frac{\epsilon(\omega)}{\epsilon_0} \right]_{\pm} = 1 + \chi_e = 1 + \frac{Ne^2}{\epsilon_0 m} \frac{1}{\omega_0^2 - \omega^2 - i\gamma\omega \pm e B_0 \omega / m}$$

$$\left(\frac{\epsilon(\omega)}{\epsilon_0} \right)_{\pm} = n_{\pm}^2, \quad \text{so } n_+^2 - n_-^2 = \frac{Ne^2}{\epsilon_0 m} \left[\frac{1}{\omega_0^2 - \omega^2 - i\gamma\omega + e B_0 \omega / m} - \frac{1}{\omega_0^2 - \omega^2 - i\gamma\omega - e B_0 \omega / m} \right]$$

(8) Consider a plane wave which propagates as the sum of 2 oppositely circularly polarized waves with a relative phase difference of ϕ . (5)

Complex field is written as $\vec{E} = E_0 \left[\frac{1}{2}(\vec{E}_1 + i\vec{E}_2) + \frac{1}{2}(\vec{E}_1 - i\vec{E}_2)e^{i\phi} \right] e^{i(kz - \omega t)}$
 \vec{E}_1, \vec{E}_2 along \hat{x} & \hat{y} respectively. (1)

at $z=0, t=0$, actual field is the real part of (1)

if $\phi=0$, $\vec{E} = E_0 \vec{E}_1$ (plane polarized along \hat{x})

$$\begin{aligned} \text{if } \phi \neq 0, \vec{E} &= \text{Re} \left\{ E_0 \left(\frac{1 + \cos \phi}{2} \vec{E}_1 + \frac{1}{2} \sin \phi \vec{E}_2 + i \left(\frac{1}{2} \vec{E}_2 + \frac{1}{2} \vec{E}_1 \sin \phi - \frac{1}{2} \vec{E}_2 \cos \phi \right) \right\} \\ &= E_0 \left[\vec{E}_1 \cos^2 \frac{\phi}{2} + \vec{E}_2 \sin \phi \cos \frac{\phi}{2} \right] = E_0 \cos \frac{\phi}{2} \left[\vec{E}_1 \cos \frac{\phi}{2} + \vec{E}_2 \sin \frac{\phi}{2} \right] \end{aligned}$$

\rightarrow plane polarized wave with polarization rotated by $\left[\frac{\phi}{2} \right]$ - (counter clockwise facing wave)

$$n_+ = \left(\frac{\epsilon_+(\omega)}{\epsilon_0} \right)^{\frac{1}{2}} \approx 1 + \frac{1}{2} \frac{Ne^2}{\epsilon_0 m} \frac{1}{(\omega_0^2 - \omega^2) + eB_0 \omega / m - i\gamma \omega} \quad (2)$$

$$n_- = \left(\frac{\epsilon_-(\omega)}{\epsilon_0} \right)^{\frac{1}{2}} = 1 + \frac{1}{2} \frac{Ne^2}{\epsilon_0 m} \frac{1}{(\omega_0^2 - \omega^2) - eB_0 \omega / m - i\gamma \omega} \quad (3)$$

Phase difference between + and - circularly polarized waves (initially zero when entering medium) given by $\frac{1}{2} kL (n_+^R - n_-^R)$ (- relative to +)

(n_{\pm}^R = Real part of n_{\pm})

(Imaginary part gives attenuation - neglect here)

$$\left(\frac{\phi}{2} \right) = -\frac{kL}{2} (n_+^R - n_-^R) = -\frac{kL}{2} \frac{1}{2} \frac{Ne^2}{\epsilon_0 m} \left[\frac{(\omega_0^2 - \omega^2) + \frac{eB_0 \omega}{m}}{(\omega_0^2 - \omega^2 + \frac{eB_0 \omega}{m})^2 + \gamma^2 \omega^2} \right]$$

$$= -\frac{(\omega_0^2 - \omega^2) - \frac{eB_0 \omega}{m}}{(\omega_0^2 - \omega^2 + \frac{eB_0 \omega}{m})^2 + \gamma^2 \omega^2} \quad \text{(Full expression)}$$

if we keep only term linear in B_0 ,

$$\left(\frac{\phi}{2} \right) \approx -\frac{kL}{2} \frac{Ne^2}{\epsilon_0 m} \frac{eB_0 \omega}{m} \frac{1}{(\omega_0^2 - \omega^2)^2 + \gamma^2 \omega^2}$$

so it rotates by $\left[\frac{\phi}{2} \right]$ clockwise facing wave.

3. (a) Maxwell's Eqs. in Medium assuming $e^{-i\omega t}$ time dependence can be written

$$\nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t} = i\omega \vec{B} \quad (1)$$

$$\nabla \times \vec{B} = \mu_0 (\nabla \times \vec{H}) = \mu_0 \frac{\partial \vec{D}}{\partial t} = -i\omega \mu_0 \epsilon_0 \left[\frac{1}{\epsilon_0} \vec{D} \right] \quad (2)$$

By (1) & (2) $\nabla \times (\nabla \times \vec{E}) = i\omega (\nabla \times \vec{B}) = \omega^2 \mu_0 \epsilon_0 \left[\frac{1}{\epsilon_0} \vec{D} \right] \quad (2)$

$$\nabla (\nabla \cdot \vec{E}) - \nabla^2 \vec{E} = \frac{\omega^2}{c^2} \left[\frac{1}{\epsilon_0} \vec{D} \right] \quad (3)$$

For our (partially) anisotropic medium, $\vec{D} = \epsilon_0 \vec{E} + \sum_{\beta} \delta \epsilon_{\alpha\beta} E_{\beta}$ (4)

$\frac{\partial}{\partial t} = k, \infty$

Eq. (3) can be written as (writing α -component of this vector Equation explicitly)

$$\left[\nabla^2 E_{\alpha} + k^2 E_{\alpha} = \nabla_{\alpha} (\nabla \cdot \vec{E}) - k^2 \sum_{\beta} \frac{\delta \epsilon_{\alpha\beta}}{\epsilon_0} E_{\beta} \right] \quad (5)$$

(b) In Eq (5) ~~the~~ R.H.S. can be regarded as a weak perturbation. \therefore formal solution in terms of Green's Function (Eq. (10.24) of Jackson) can be written as

$$\vec{E}_{\alpha} = \vec{E}_{\alpha}^{(0)} + \frac{1}{4\pi} \int d^3x' \frac{e^{ik|\vec{x}-\vec{x}'|}}{|\vec{x}-\vec{x}'|} \left\{ \nabla_{\alpha} (\nabla \cdot \vec{E}) - k^2 \sum_{\beta} \frac{\delta \epsilon_{\alpha\beta}}{\epsilon_0} E_{\beta} \right\} \quad (6)$$

Far field solution is of form

$E_{\alpha} \rightarrow E_{\alpha}^{(0)} + \vec{A}_{\alpha\beta} \frac{e^{ikr}}{r}$ (by analogy with (10.26) of Jackson)

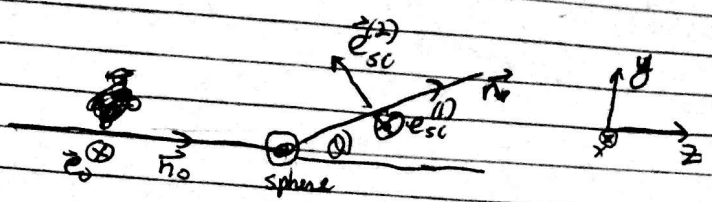
we $\int \frac{A_{\alpha\beta}}{4\pi} \int d^3x' e^{-ik\vec{r} \cdot \vec{x}'} \left\{ \nabla_{\alpha} (\nabla \cdot \vec{E}) - k^2 \sum_{\beta} \frac{\delta \epsilon_{\alpha\beta}}{\epsilon_0} E_{\beta} \right\} \quad (7)$

First term can be reduced to a surface integral over finite size of medium & vanishes since $\nabla \cdot \vec{E} = 0$ in free space

Born Approxⁿ choose E_{β} to be incident field, $E_{\beta}^{(0)} = \vec{e}_{\alpha\beta} e^{ik\vec{r}_0 \cdot \vec{x}'}$

Eq. (7) gives $\vec{A}_{\alpha\beta} \cdot \vec{e}_{\alpha\beta} = -\frac{k^2}{4\pi} \int d^3x' e^{i\vec{q} \cdot \vec{x}'} \sum_{\alpha\beta} (\vec{e}_{\alpha\beta})_{\alpha} \frac{\delta \epsilon_{\alpha\beta}}{\epsilon_0} (\vec{e}_{\alpha\beta})_{\beta}$

(b)



In this case, $\vec{e}_0 = (1, 0, 0)$; $\vec{e}_{oc} = (1, 0, 0)$; $\vec{e}_{sc} = (0, \sin\theta, \cos\theta)$

$$\vec{q} = k(\vec{n} - \vec{n}_0) \quad |\vec{q}| = q = 2k \sin(\frac{\theta}{2})$$

$$\left(\frac{d\sigma}{d\Omega}\right)^{(1)} = \frac{|\vec{A}_{sc} \cdot \vec{e}_{sc}^{\perp}|^2}{|E_0|^2} = \frac{k^4}{16\pi^2} \left| \frac{\delta \epsilon_{xx}}{\epsilon_0} \right|^2 \left| \int_{\text{sphere}} e^{i\vec{q} \cdot \vec{x}'} d^3x' \right|^2$$

from given form for $\frac{\delta \epsilon_{xx}}{\epsilon_0}$ }
$$= \frac{k^4 A^2}{16\pi^2 \epsilon_0^2} \left[\frac{4\pi^2 \delta \sin(qa) - (qa) \cos(qa)}{3qa^3} \right]^2$$

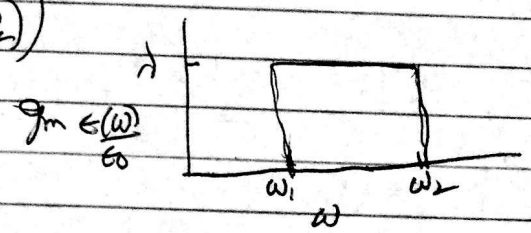
$$= \frac{k^4 A^2 a^3}{9\epsilon_0^2} \left[\frac{\sin(qa) - (qa) \cos(qa)}{qa^3} \right]^2 \quad \text{for } \vec{e}_{sc} \parallel \text{to } x\text{-axis}$$

$$\left(\frac{d\sigma}{d\Omega}\right)^{(2)} = \frac{k^4}{16\pi^2} \left| \frac{\delta \epsilon_{yx}}{\epsilon_0} + \frac{\delta \epsilon_{zy}}{\epsilon_0} \right|^2 \left| \int_{\text{sphere}} e^{i\vec{q} \cdot \vec{x}'} d^3x' \right|^2$$

$$= \frac{k^4}{16\pi^2} \left| iBM_x - iBM_y \right|^2 \left| \int_{\text{sphere}} e^{i\vec{q} \cdot \vec{x}'} d^3x' \right|^2$$

(only M_z exists) = 0 for $\vec{e}_{sc} \perp$ to x -axis

(4) $\text{Im} \left(\frac{\epsilon(\omega)}{\epsilon_0} \right) = \lambda \left(\delta(\omega - \omega_1) - \delta(\omega - \omega_2) \right)$



By Kramers-Kronig, Eq. (7.120) of Jackson

$$\text{Re} \left(\frac{\epsilon(\omega)}{\epsilon_0} \right) = 1 + \frac{2\lambda}{\pi} \mathcal{P} \int_0^{\omega} \frac{\omega' \text{Im}(\epsilon(\omega')/\epsilon_0)}{\omega'^2 - \omega^2} d\omega'$$

$$= 1 + \frac{2\lambda}{\pi} \mathcal{P} \int_{\omega_1}^{\omega_2} \frac{\omega'}{\omega'^2 - \omega^2} d\omega' = 1 + \frac{\lambda}{\pi} \left[\ln \left| \frac{\omega_2^2 - \omega^2}{\omega_1^2 - \omega^2} \right| \right]$$

(substitute $z = \omega'^2$)

